

Aerodynamics of Bristled Wings

Yukesh Karki¹ and Chandan Bose²

¹UG Research Scholar, Dept. of Mechanical and Aerospace Engineering, Tribhuvan University, IOE, Pulchowk Campus

²Assistant Professor, Aerospace Engineering, College of Engineering and Physical Sciences, The University of Birmingham

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Synopsis

Microscopic flying insects like thrips and fairyflies possess a distinct wing structure characterized by several bristles extending from a main frame. At low Reynolds numbers of $O(10)$, bristled wings exhibit enhanced aerodynamic efficiency compared to solid membranous wings. This study presents a numerical investigation of bristled wing models at two different angles of attack and a Reynolds number of 30 using the open-source computational fluid dynamics (CFD) package OpenFOAM. Three bristled wing geometries with 4, 5 and 6 bristles were examined. Results indicate that force coefficients increased with the number of bristles, while decreasing gap width between bristles minimized flow leakage through strong viscous diffusion, creating a virtual fluid barrier resulting it to act like a membranous wing. Among the studied bristled wing models, the 6-bristled wing model demonstrated comparable drag to the solid wing model despite its smaller surface area. However, achieving an optimal bristled wing configuration requires a systematic investigation comparing various wing models with different bristle numbers based on generated lift, drag, lift-to-drag ratio, and other parameters.

1 Introduction

Microscopic insects like thrips and fairyflies, measuring 300 to 1000 microns in length, have long puzzled scientists with their ability to fly. Initially, it was believed that they merely drifted with the wind. However, recent studies have shown that these tiny insects can fly very well, displaying great maneuverability in the air. To sustain flight, these insects must generate enough lift to counteract their entire body weight. Previous research conducted by Santhanakrishnan et. al. [1] demonstrated that when a solid elliptical wing maintains a constant revolution at a steady angle of attack (AOA), drag experiences a substantial increase with decreasing Reynolds number, while the increase in lift appears to be minimal as illustrated in Figure 1.

In order to overcome the challenge posed by these heightened drag forces, microscopic insects have evolved bristled wings [2–5]. Bristled wings consist of multiple cylindrical bristles extending

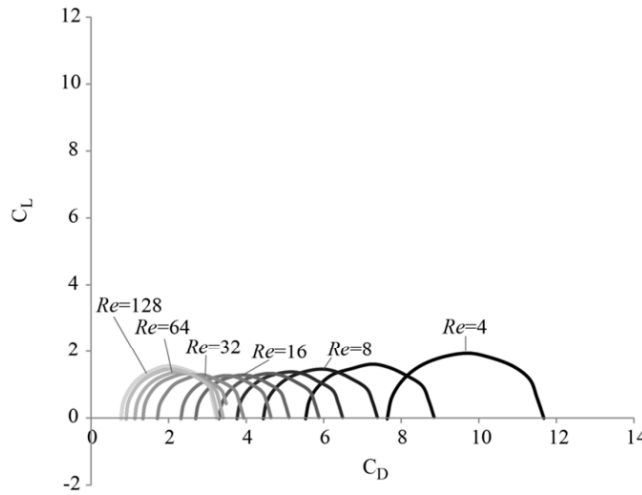


Figure 1: C_L vs C_D for over a range of Re [1].

from a main frame, forming a discontinuous surface having gaps between the bristles as can be seen in figure presented in the work of Huber et. al. [6]. The simplified 2D representation of a bristled wing is shown in Figure 2. At high Reynolds numbers, the array demonstrates rake-like behavior. However at very low Reynolds numbers, the array of hairs behaves like paddles, with minimal fluid leakage between them.



Figure 2: 2D bristled wing model [5].

Sunada et. al. [7] conducted experimental research on solid and bristled wing model. They showed that the hairy structure of bristled wing exert forces similar to those of equivalent solid wing, thus reducing the mass of an insect. Similarly, Lee et. al. [8] conducted experiments on comb-like plate, focusing on viscous diffusion. At a low Reynolds number of $O(10)$, shear layers generated at the tooth edges diffused strongly blocking the gaps between the teeth. This blockage increased the effective surface area of the plate, altering the formation of leading and trailing edge vortices and resulting in larger aerodynamic forces. Lee et al. [3] numerically investigated the optimal configuration of 2D bristled wings, adjusting the Reynolds number calculated on the basis of bristle diameter (Re_b) and gap width between the bristles. They showed that the flow blockage was increased with decreasing Re_b and decreased with increasing gap width. Additionally, Lee et

al. [2] performed a 2D numerical study on bristled wing models to examine gap flow formation during unsteady deceleration and stroke reversal. In the study conducted by Wu et. al. [5], the drag production mechanism was studied for solid wing and bristled wing. When the bristle number reached a certain value, they showed that there is little to no effect on force production with further increase in bristles with the disadvantage of increasing mass.

In the present study, the flow structure on bristled wing model with 4, 5 and 6 numbers of bristle is numerically investigated at the Reynolds number of 30 based on chord length and compared it with the equivalent solid wing having same aspect ratio. By varying the number of bristles, the aerodynamic performance based on flow structure is evaluated as the gap width between the bristles changes. Two different angle of attack of 90° and 45° is also taken into account for this study to investigate the nature of flow structure and its aerodynamic performance due to changing angle of attack.

2 Governing Equations and Models

2.1 Problem definition

This study investigates the aerodynamic performance of a bristled wing model compared to a solid wing at a Reynolds number of 30 using 2D numerical simulations. This project aims to analyze the influence of bristles on lift, drag and flow phenomena through simulations to evaluate their potential for improved flight performance.

Three bristle wing models are considered with 4, 5 and 6 number of bristles having bristle diameter 10% of L (where L is the chord length of the wing). The equivalent solid wing is also considered for comparison having thickness same as that of the bristle diameter (i.e. 10% of L) with semi-circular leading and trailing edges as seen in Figure 3.

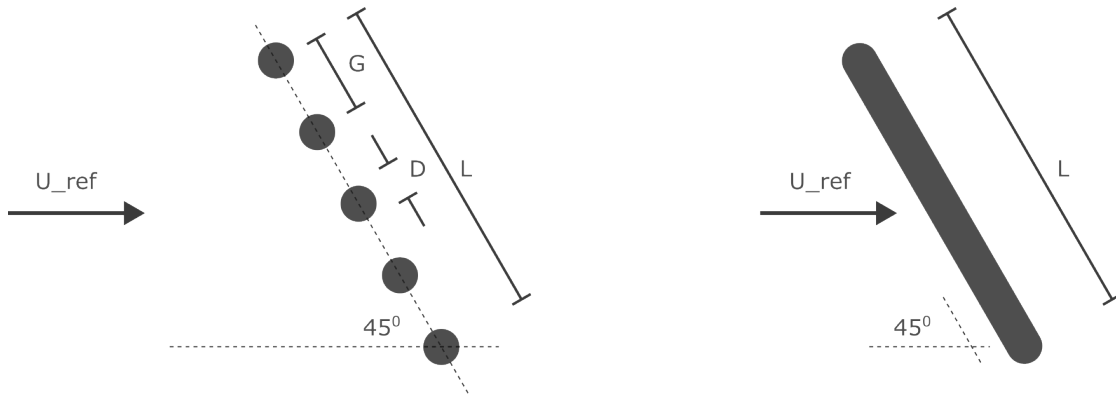


Figure 3: Schematic diagrams of bristled wing model (left) and corresponding solid wing model (right)

2.2 Governing equations

The flow around the model wing is governed by the incompressible Navier-Stokes equations.

Continuity Equation:

$$\nabla \cdot \mathbf{u} = 0 \quad (1)$$

Momentum Equation:

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot (\nabla \cdot \mathbf{u}) = -\frac{1}{\rho} (\nabla \cdot p) + \nu \nabla^2 \cdot \mathbf{u} \quad (2)$$

where ρ is the density, ν is the kinematic viscosity, \mathbf{u} is the velocity vector and p is the pressure. pimpleFoam, a pressure-based transient, incompressible solver is selected for this study. It employs the PIMPLE algorithm, which combines PISO and SIMPLE methods for pressure-momentum coupling. Turbulence modelling is not performed due to the laminar nature of the flow.

2.3 Geometry and Mesh

blockMesh utility, OpenFOAM's built-in tool, is used to model and discretize the geometry.

2.3.1 Bristle Wing

The computational domain consists 391 vertices and 169 blocks for the domain with 5 bristles wing model. The schematic diagram of the computational domain is shown in Figure 4 and the bristled wing parameters are given in Table 1. The G/D ratio for 4, 5 and 6 number of bristles wing model are 3.33, 2.5 and 2 respectively.

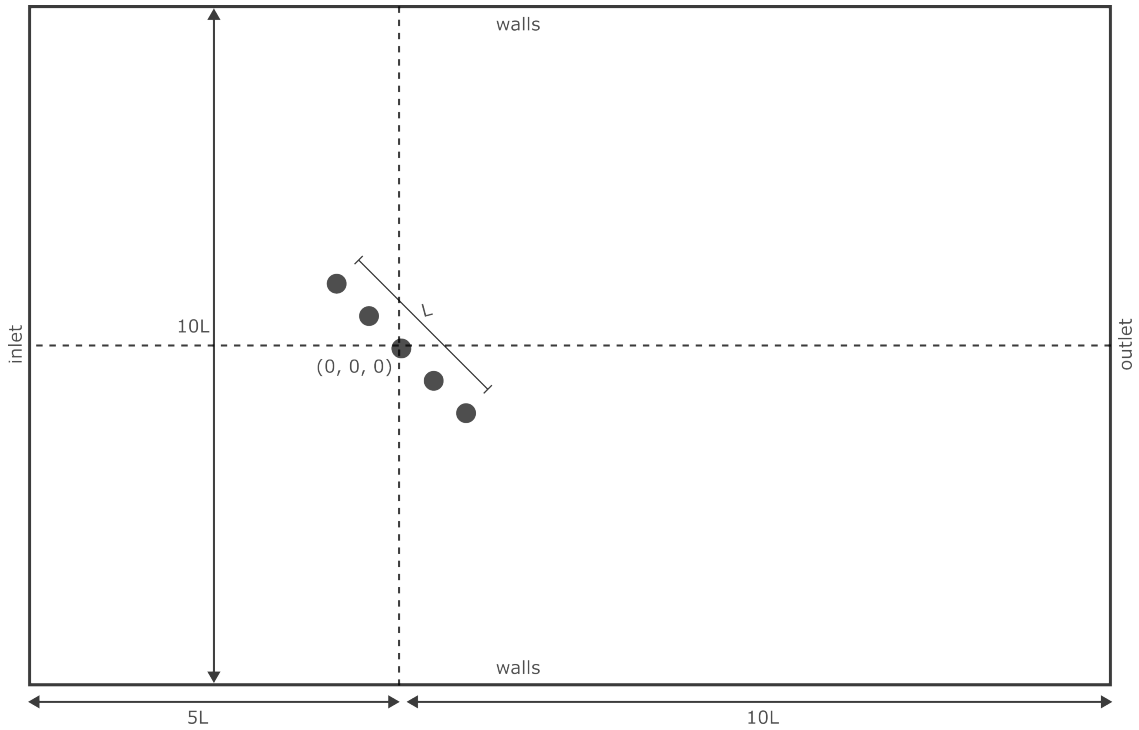


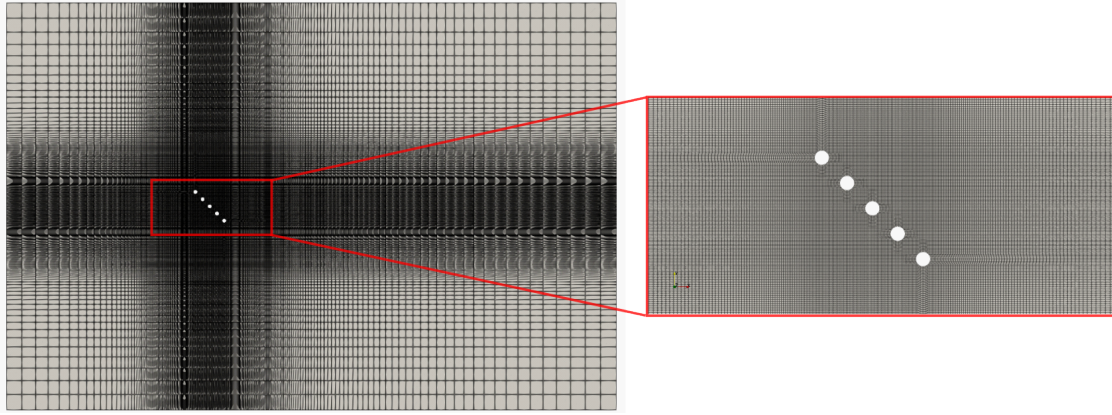
Figure 4: Computational Domain

Table 1: Parameters for 5-Bristled Wing Model

| Parameters | Value | Unit |
|--------------------------|-------|-------|
| Chord Length (L) | 1 | meter |
| Diameter of bristles (D) | 0.1 | meter |
| Gap width (G) | 0.25 | meter |

The computational domain with dimensions of $15L$ in stream wise direction ($-5 < x/L < 10$), and $10L$ in normal direction ($-5 < y/L < 5$) with the center of wing as origin is adapted in this study.

A grid convergence test was conducted to finalize the grid size, as detailed in Section 3.1. The converged mesh has 73,705 hexahedral elements, shown in Figure 5.

Figure 5: Computational Mesh for bristled wing at 45° AOA

The same converged mesh sizing is used for geometries with 4 and 6 number of bristles as shown in Figure 6 and 7.

Similarly, using the same converged mesh parameters, the mesh is created for geometry with 90° AOA shown in Figure 8, 9 and 10.

2.3.2 Solid Wing

Similar domain was created for solid wing with equivalent chord length. The computational domain consists 89 vertices and 34 blocks. The converged mesh has 43608 hexahedral elements, shown in Figure 11.

Similarly, the mesh created for geometry with 90° AOA is shown in Figure 12.

2.4 Solver setup

The 2D incompressible laminar flow over the bristled wing model is solved numerically using OpenFOAM v2112.

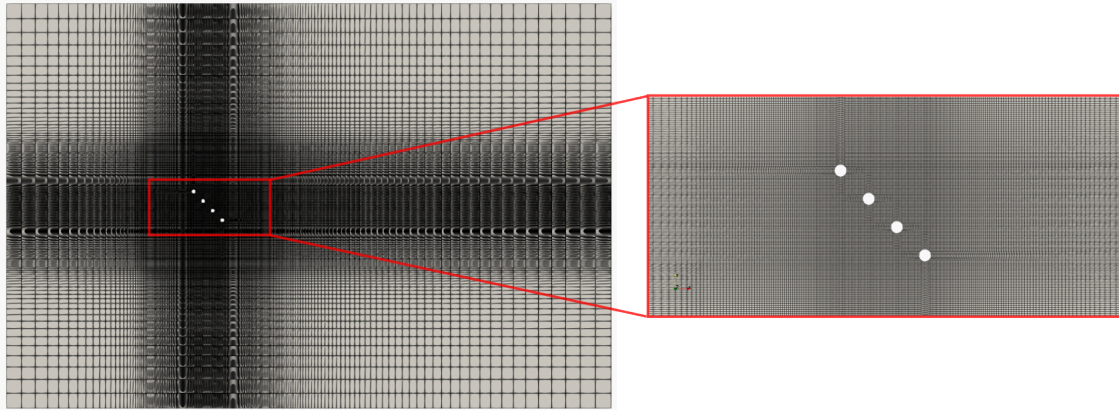


Figure 6: Computational Mesh for 4 bristled wing model at 45°AOA

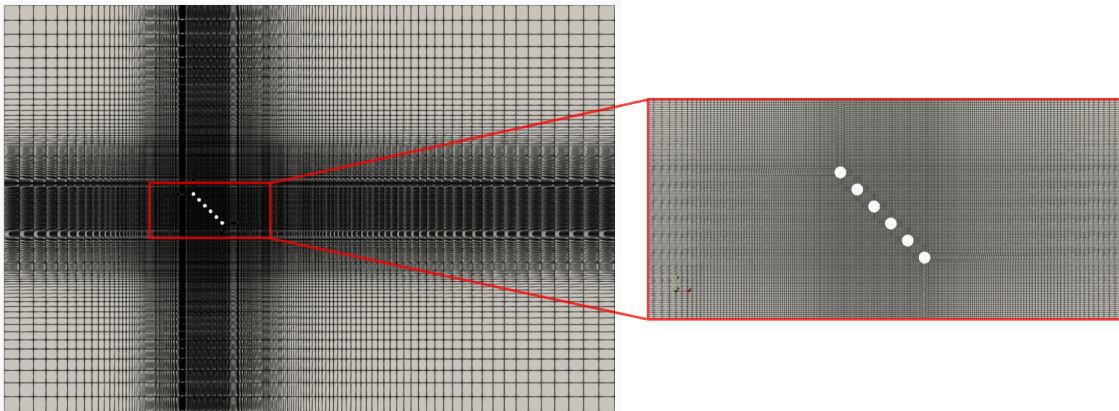


Figure 7: Computational Mesh for 6 bristled wing model at 45°AOA

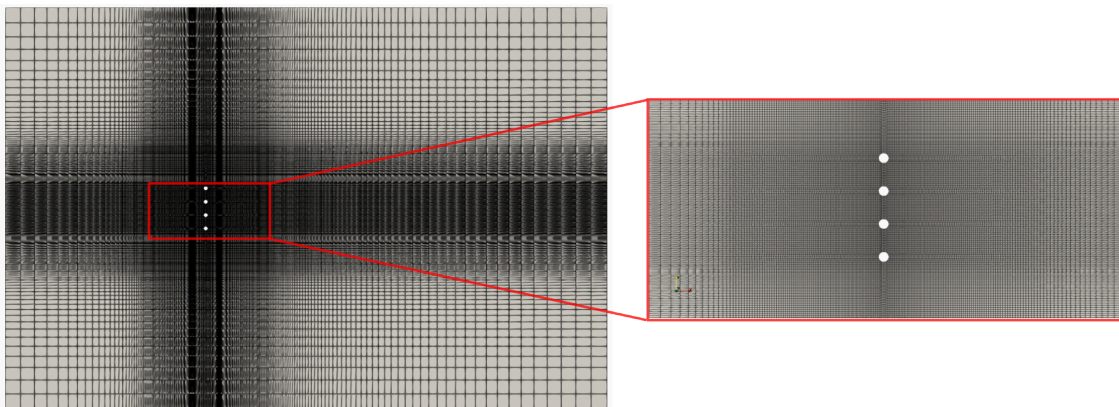


Figure 8: Computational Mesh for 4 bristled wing at 90°AOA

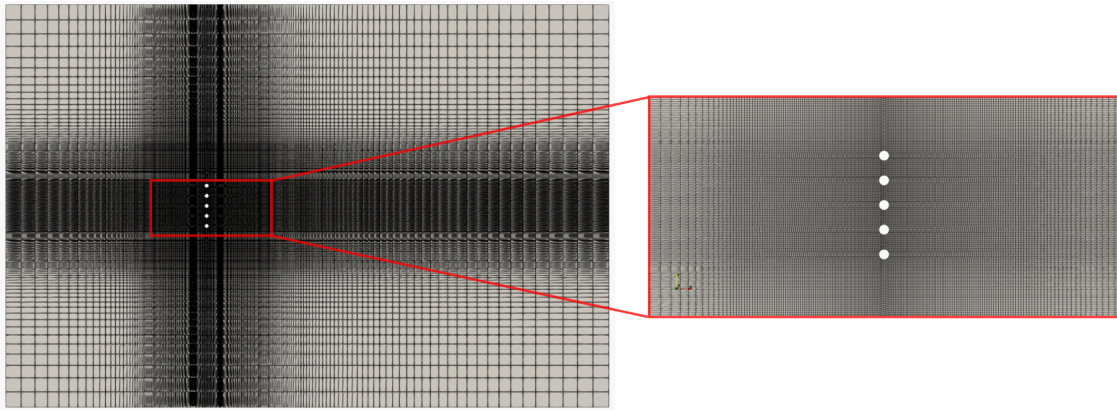


Figure 9: Computational Mesh for 5 bristled wing at 90° AOA

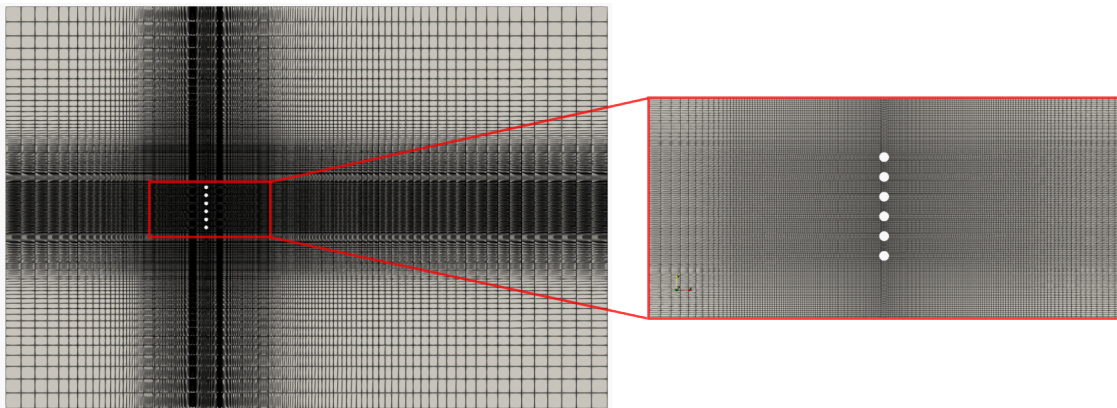


Figure 10: Computational Mesh for 6 bristled wing at 90° AOA

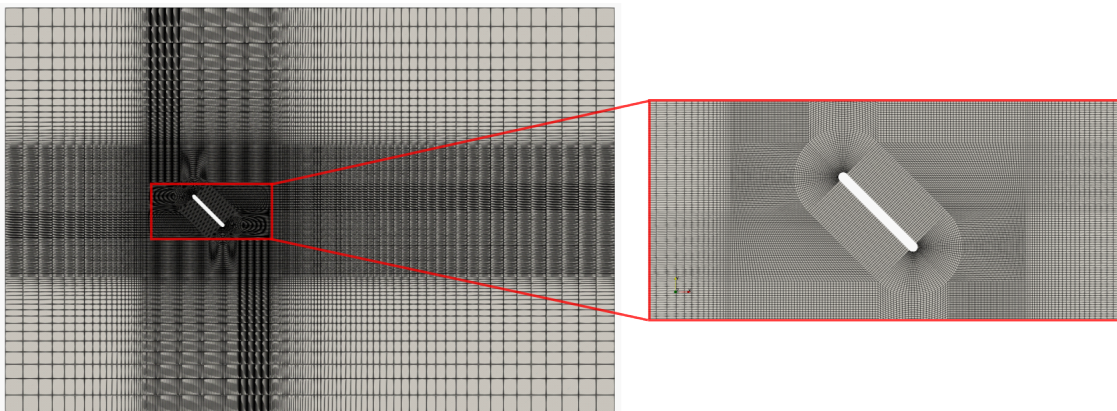


Figure 11: Computational Mesh for solid wing at 45° AOA

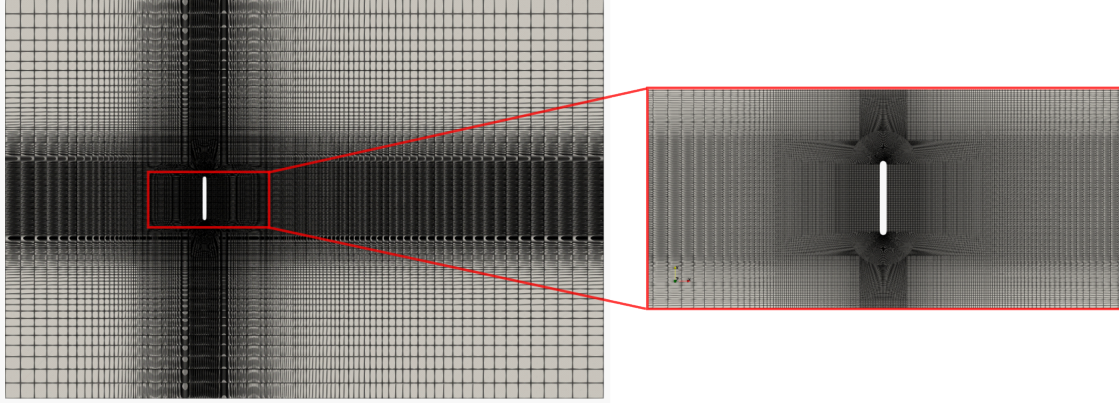


Figure 12: Computational Mesh for solid wing at 90° AOA

2.4.0.1 Fluid Properties

For this study, a theoretical fluid is utilized. To obtain a Reynolds number (Re) of 30 based on chord length, with a constant inlet velocity of 1 m/s , the kinematic viscosity (ν) is adjusted while maintaining a constant chord length (L) of 1 m . The formula for calculating Reynolds Number (Re) is given as:

$$Re = \frac{UL}{\nu} \quad (3)$$

where U is the free-stream inlet velocity, ν is the kinematic viscosity and L is the chord length. Hence, the calculated kinematic viscosity (ν) is $0.033 \text{ m}^2/\text{s}$. Reynolds number calculated based on bristle diameter (Re_b) is given as:

$$Re_b = \frac{UD}{\nu} \quad (4)$$

where D is the bristle diameter and the corresponding Reynolds number calculated based on bristle diameter (Re_b) is 3.

2.4.0.2 Porosity

The area that the bristles occupy divided by the area of a equivalent solid wing is known as the porosity of the model wing.

$$Porosity = \frac{A_{bristles}}{A_{solid}} \quad (5)$$

where $A_{bristles}$ is the total area occupied by the bristles in model bristle wing and A_{solid} is the total area of an equivalent solid wing.

2.4.0.3 Dimensionless Forces

The forces experienced by the model wing were non-dimensionalized by $0.5\rho U^2 L$ to compare the forces obtained from the numerical simulation. The coefficients of lift and drag are denoted by C_l and C_d , respectively.

2.4.0.4 Initial and Boundary Conditions

Four boundaries (inlet, outlet, walls and wing) are defined in the blockMeshDict file. The initial and boundary conditions are shown in Table 2, 3 and 4.

Table 2: Initial Conditions

| Flow Variable | Value |
|---------------|----------------------------|
| U | 0 m/s |
| p | $0 \text{ m}^2/\text{s}^2$ |

Table 3: Boundary Condition for p

| Patch | Condition | Value (m^2/s^2) |
|--------------|--------------|-----------------------------------|
| inlet | zeroGradient | - |
| outlet | fixedValue | 0 |
| walls | zeroGradient | - |
| wing | zeroGradient | - |
| defaultFaces | empty | - |

Table 4: Boundary Condition for U

| Patch | Condition | Value (m/s) |
|--------------|--------------|------------------------|
| inlet | fixedValue | (1, 0, 0) |
| outlet | zeroGradient | - |
| walls | slip | - |
| wing | noSlip | - |
| defaultFaces | empty | - |

2.4.0.5 Equation Discretization

In OpenFOAM, Finite Volume Method (FVM) is used to discretize and solve the continuum equations. After mesh generation, the NS equation given in equation (1, 2) are to be solved on those individual cells. This is generally composed of temporal, spatial and equation schemes.

Equation discretization defines the computational methods used on the conservation laws for a specific time-step and location, described by the temporal and spatial discretization. The discretization schemes used in this study is given in Table 5.

Table 5: Discretization Schemes

| Discretization | Scheme | Order of accuracy |
|----------------|------------------------|-------------------|
| Temporal | Euler | First |
| Gradient | Gauss linear | Second |
| Laplacian | Gauss linear corrected | Second |
| Interpolation | Linear | Second |

2.4.0.6 Solution Method and Control

The solvers used in the study is shown in Table 6. For PIMPLE algorithm, two correction steps are used within a single time-step and does not utilize any non-orthogonal correctors. A flow time step of $1e-4$ has been chosen for the simulation. .

Table 6: Numerical Solvers

| Field | Linear Solver | Smoother | Tolerance |
|-------|---------------|---------------------------------|-----------|
| p | GAMG Solver | DIC Gauss Seidel Smoother | $1e-6$ |
| U | Smooth Solver | Symmetric Gauss Seidel Smoother | $1e-5$ |

3 Results and Discussions

3.1 Grid Size Convergence Test

3.1.1 Bristle Wing

Four mesh sizing were taken for grid size convergence study. Coefficient of drag (C_d) and coefficient of lift (C_l) over the wing model was selected as the convergence test parameter.

Richardson extrapolation method given by Roache [9] is used to calculate the exact value of C_d and C_l taking the three most refined cases. This method calculates the exact value of the test parameter as the grid spacing tends to 0 (i.e. $\Delta x \rightarrow 0$ and $\Delta y \rightarrow 0$).

The constant grid refinement ration (r) is approximately set to 2.

The result of grid convergence test is shown in Table 7 and 8.

The exact value of coefficient of drag (C_d) and lift (C_l) obtained was 1.72512 and 0.770488 respectively. Taking the factor of safety value as 1.5, the calculated Grid Convergence Index (GCI) is given in Table 9.

Table 7: Grid Convergence Study using C_d

| Grid level | Number of Elements | Coefficient of drag (C_d) | Error | Error (%) |
|--------------------------|--------------------|-------------------------------|---------|-----------|
| M1 | 16774 | 1.71857 | 0.00655 | 0.379684 |
| M2 | 35629 | 1.72277 | 0.00235 | 0.136222 |
| M3 | 73705 | 1.72497 | 0.00015 | 0.008695 |
| M4 | 145564 | 1.72511 | 0.00001 | 0.00058 |
| Richardson Extrapolation | - | 1.72512 | - | - |

Table 8: Grid Convergence Study using C_l

| Grid level | Number of Elements | Coefficient of lift (C_l) | Error | Error (%) |
|--------------------------|--------------------|-------------------------------|----------|-----------|
| M1 | 16774 | 0.72801 | 0.042478 | 5.513129 |
| M2 | 35629 | 0.75116 | 0.019328 | 2.50854 |
| M3 | 73705 | 0.76392 | 0.006568 | 0.852447 |
| M4 | 145564 | 0.7682 | 0.002288 | 0.296955 |
| Richardson Extrapolation | - | 0.770488 | - | - |

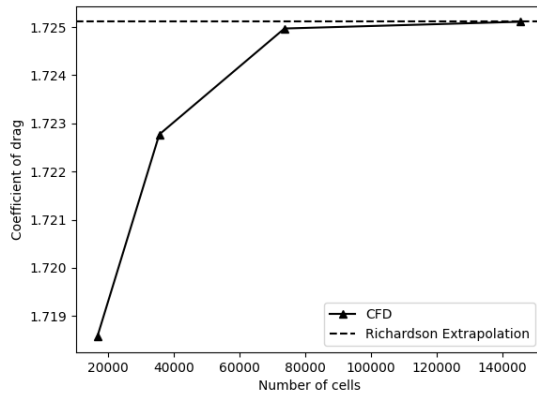
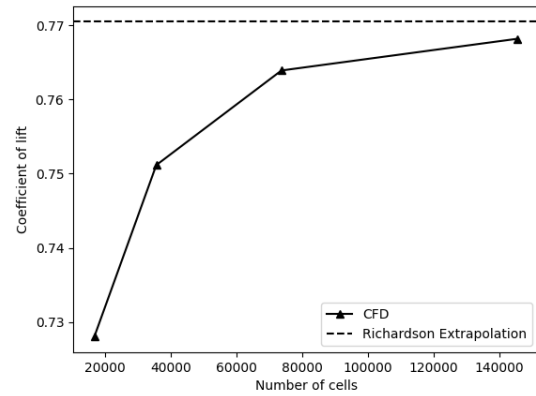
(a) Coefficient of Drag (C_d)(b) Coefficient of Lift (C_l)

Figure 13: Richardson Extrapolation for 5 Bristle Wing Model

Table 9: Grid Convergence Index

| | Coefficient of drag (C_d) | Coefficient of lift (C_l) |
|------------------|-------------------------------|-------------------------------|
| Coarse to Medium | 0.011% | 1.116% |
| Medium to Fine | 0.0008% | 0.4136% |

Table 10: Converged Mesh's Parameters for Bristled wing

| | Min $\Delta x(m)$ | Max $\Delta x(m)$ | Min $\Delta y(m)$ | Max $\Delta x(m)$ |
|----------------------|-------------------|-------------------|-------------------|-------------------|
| Inside Bounding Box | 0.0101 | 0.0101 | 0.0101 | 0.0101 |
| Outside Bounding Box | 0.0101 | 0.1467 | 0.0101 | 0.14 |

The M3 mesh is assumed to be converged as it is within the asymptotic range of convergence and is taken for further study. The converged mesh's parameters are tabulated in Table 10. The mesh consists of 73705 total cells. The maximum skewness of the mesh is 0.5491 with a maximum non-orthogonality of 38.45°.

3.1.2 Solid Wing

Similar approach was taken for studying the grid convergence for solid wing as well. The results of grid convergence study for solid wing is given in Table 11 and 12.

Table 11: Grid Convergence Study using C_d

| Grid level | Number of Elements | Coefficient of drag (C_d) | Error | Error (%) |
|--------------------------|--------------------|-------------------------------|---------|-----------|
| M1 | 10752 | 1.72667 | 0.02237 | 1.27899 |
| M2 | 22145 | 1.73706 | 0.01198 | 0.68495 |
| M3 | 43608 | 1.74205 | 0.00699 | 0.39965 |
| M4 | 86740 | 1.74498 | 0.00406 | 0.23213 |
| Richardson Extrapolation | - | 1.74904 | - | - |

Table 12: Grid Convergence Study using C_l

| Grid level | Number of Elements | Coefficient of lift (C_l) | Error | Error (%) |
|--------------------------|--------------------|-------------------------------|---------|-----------|
| M1 | 10752 | 1.14776 | 0.01384 | 1.19146 |
| M2 | 22145 | 1.15313 | 0.00847 | 0.72197 |
| M3 | 43608 | 1.15609 | 0.00551 | 0.47435 |
| M4 | 86740 | 1.15803 | 0.00357 | 0.30733 |
| Richardson Extrapolation | - | 1.1616 | - | - |

The calculated GCI is shown in Table 13.

Figure 14 shows the grid convergence plots for solid wing.

Table 13: Grid Convergence Index

| | Coefficient of drag (C_d) | Coefficient of lift (C_l) |
|------------------|-------------------------------|-------------------------------|
| Coarse to Medium | 0.4959% | 0.5885% |
| Medium to Fine | 0.2852% | 0.3782% |

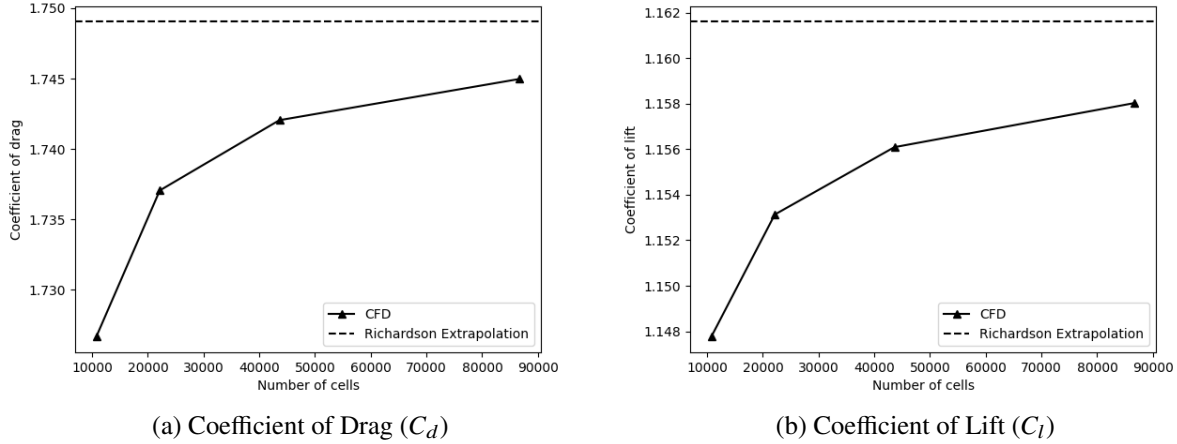


Figure 14: Richardson Extrapolation for Solid Wing Model

The M3 mesh is assumed to be converged as it is within the asymptotic range of convergence and is taken for further study. The converged mesh's parameters are tabulated in Table 14. The mesh consists of 43608 total cells. The maximum skewness of the mesh is 0.6559 with a maximum non-orthogonality of 44.728° .

Table 14: Converged Mesh's Parameters for Bristled wing

| | Min $\Delta x(m)$ | Max $\Delta x(m)$ | Min $\Delta y(m)$ | Max $\Delta y(m)$ |
|----------------------|-------------------|-------------------|-------------------|-------------------|
| Inside Bounding Box | 0.02828 | 0.02828 | 0.02828 | 0.02828 |
| Outside Bounding Box | 0.02828 | 0.46 | 0.02828 | 0.46 |

3.2 Results

3.2.1 Aerodynamic Forces at $\alpha = 90^\circ$

For comparing the forces between the model wings, the non-dimensional drag or drag coefficient (C_d) and the non-dimensional lift or lift coefficient (C_l) are defined. The computed drag coefficients for wing model at 90° AOA is shown in Figure 15 and the values are given in Table 15. Figure 16 shows velocity contour with streamlines pattern around the wing.

The solid wing has the highest value of C_d of 2.44599. The two weak counter-rotating vortices at the back of the solid wing can be seen on Figure 16 which are formed due to the flow separation

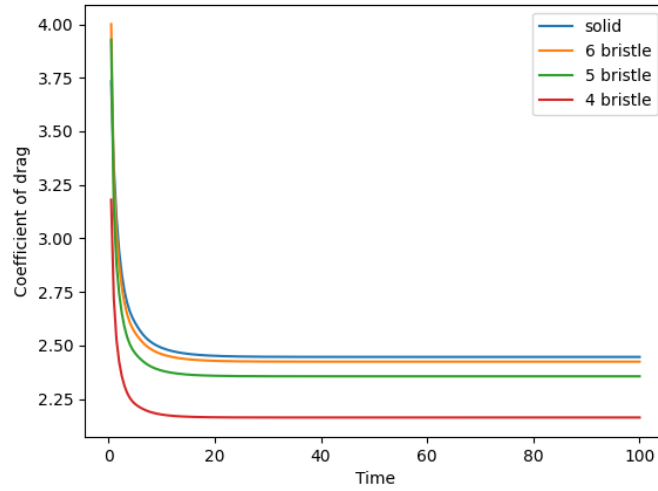


Figure 15: Coefficient of drag at 90° AOA

Table 15: Coefficients of drag for the model wings at 90° AOA

| | Solid wing | Six-bristled wing | Five-bristled wing | Four-bristled wing |
|-------|------------|-------------------|--------------------|--------------------|
| C_d | 2.44599 | 2.42401 | 2.35547 | 2.16304 |

occurring at leading and trailing edges of the wing. As a result, the solid wing's front surface experiences positive pressure, and its rear surface experiences negative pressure due to the two back vortices. Hence, large drag is experienced for solid wing model.

For six-bristled wing model, it is seen that the size of vortex behind the wing is smaller than that of the solid wing which significantly reduces for five-bristle wing and finally vanishes for four-bristle wing model. The result also shows that the value of C_d decreases as the number of bristles decreases. For 4-bristle wing model, C_d is 2.16304 which is lowest among all. The obtained C_d for model wing with 6 and 5 number of bristles are 2.42401 and 2.35547 respectively.

Vorticity contour for all the model wings are shown in Figure 17, where the blue and red color indicate the clockwise and counter-clockwise direction respectively. The two counter-rotating vortices can be seen in Figure 17a for solid wing. For bristle wing, each individual bristle operates within a creeping flow regime, as noted by Rajani et al. [10] for Re_b of 3. This results in the formation of strong shear layers around each bristle, preventing flow separation. The vorticity within the gaps between bristles is annihilated by vorticity of opposite sign generated by adjacent bristles due to strong viscous diffusion. As a result, the vorticity inside the gaps is not as strong as the vorticity at the extreme edges of the wing. (Figure 17b, 17c and 17d). The 6-bristled wing's leading and trailing edge vortices are similar in size and magnitude to the equivalent solid wing depicted in Figure 17a. Thus 6-bristled wing experience nearly equal drag force than that of solid wing.

As the number of bristles decreases, the gap width increases which decreases the interference effect as can be seen in Figure 17c and 17d. Hence lower drag is experience by 4-bristled wing as more flow can pass through the gap.

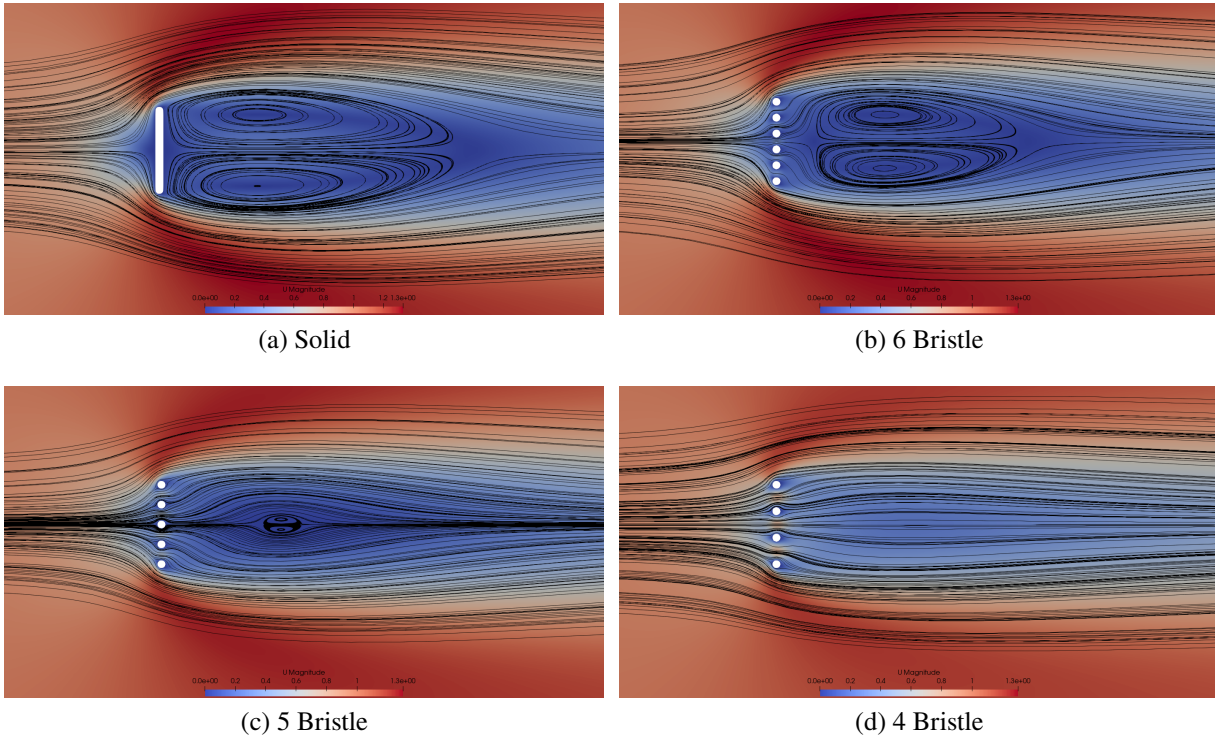


Figure 16: Velocity Contour with streamlines at 90° AOA

3.2.2 Effect of Angle of Attack

In the study on flow dynamics between gill rakers [11], the authors found that the velocity and angle of attack of the flow are crucial in forming vortices. These vortices reduce the effective gap size between the rakers, thereby altering the leakiness. In the study conducted by Jones et. al. [12], similar variation in leakiness with changes in the AOA was observed when the bristled wing was translated at 45° angle of attack. When the number of bristles were reduced, the calculated force coefficients decreased as well. At angles of attack close to 45°, this effect was largest for lift, and at angles of attack close to 90°, for drag.

Vorticity contour and velocity streamlines for wings at 45° AOA are shown in Figure 18 and 19 respectively.

In the case of a solid wing, the fluid flows entirely around its outer edges since it cannot pass through the surface. As a result, the leading edge vortex on the solid wing is fully developed. However, for bristled wing model, each bristle generates a pair of counter-rotating vortices. These vortices exhibit greater size and magnitude near both edges of the wing. At an angle of attack of 45°, vortices disperse more widely, covering a larger area. This dispersion effectively diminishes the gap between the bristles, which alters the interference effect and the volume of fluid which passes through it.

Observing the streamline pattern, it can be seen that more fluid is passed through the gap near the leading edge compared to the gap near the trailing edge. This is due to change in effective length near trailing edge due to the superimposition of the shear layer. Thus large separation region near trailing edge can be seen behind the 6-bristled wing model (Figure 19b). As the number of bristle

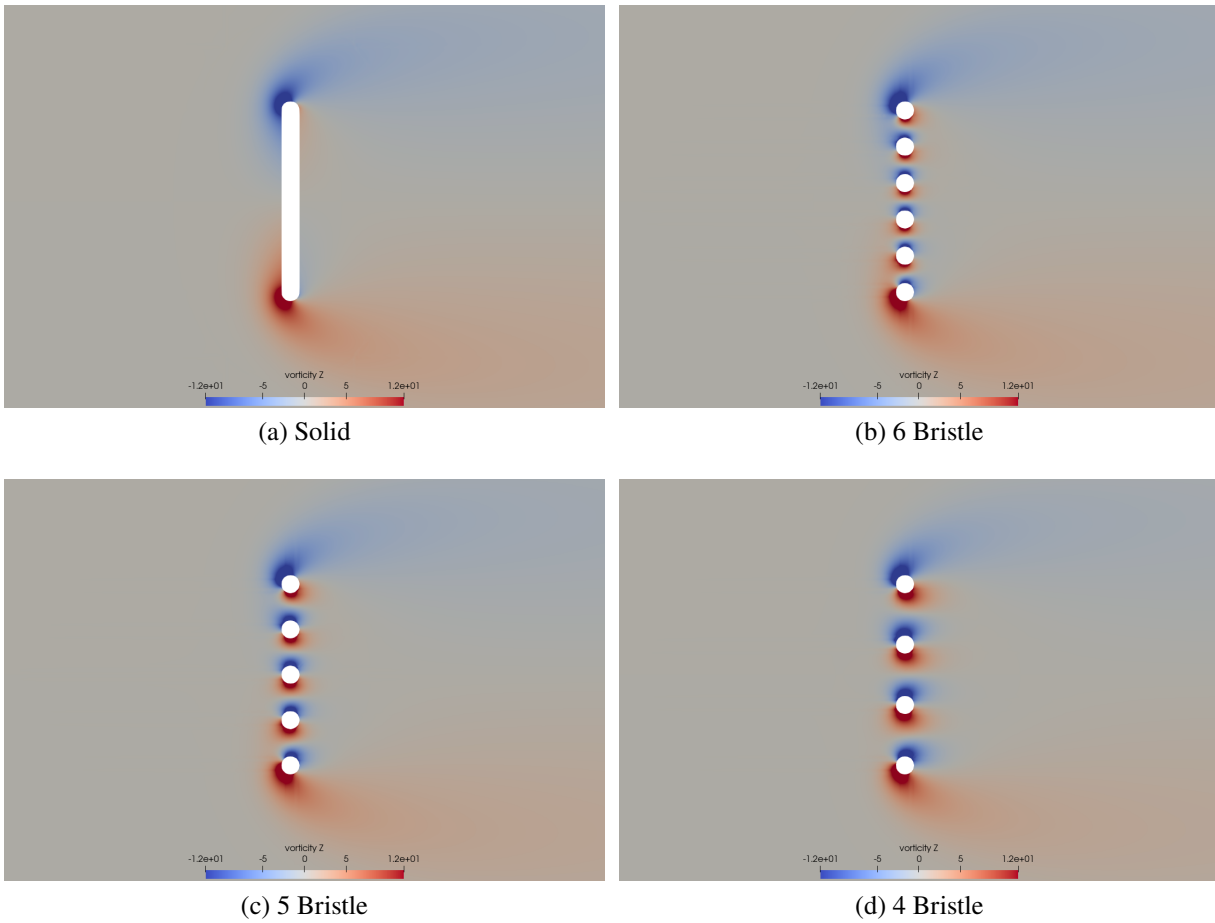


Figure 17: Vorticity contour at 90° AOA

decreases, it can be seen that the interference effect decreases and more fluid is able to pass through the gap even at 45° AOA. This explains the larger lift to drag ratio for 6-bristled wing model than that of 4-bristled wing model.

Figure 20 shows the force coefficients comparison for all the model wings obtained from simulation. The obtained value of C_d and C_l with their corresponding C_l/C_d are given in Table 16.

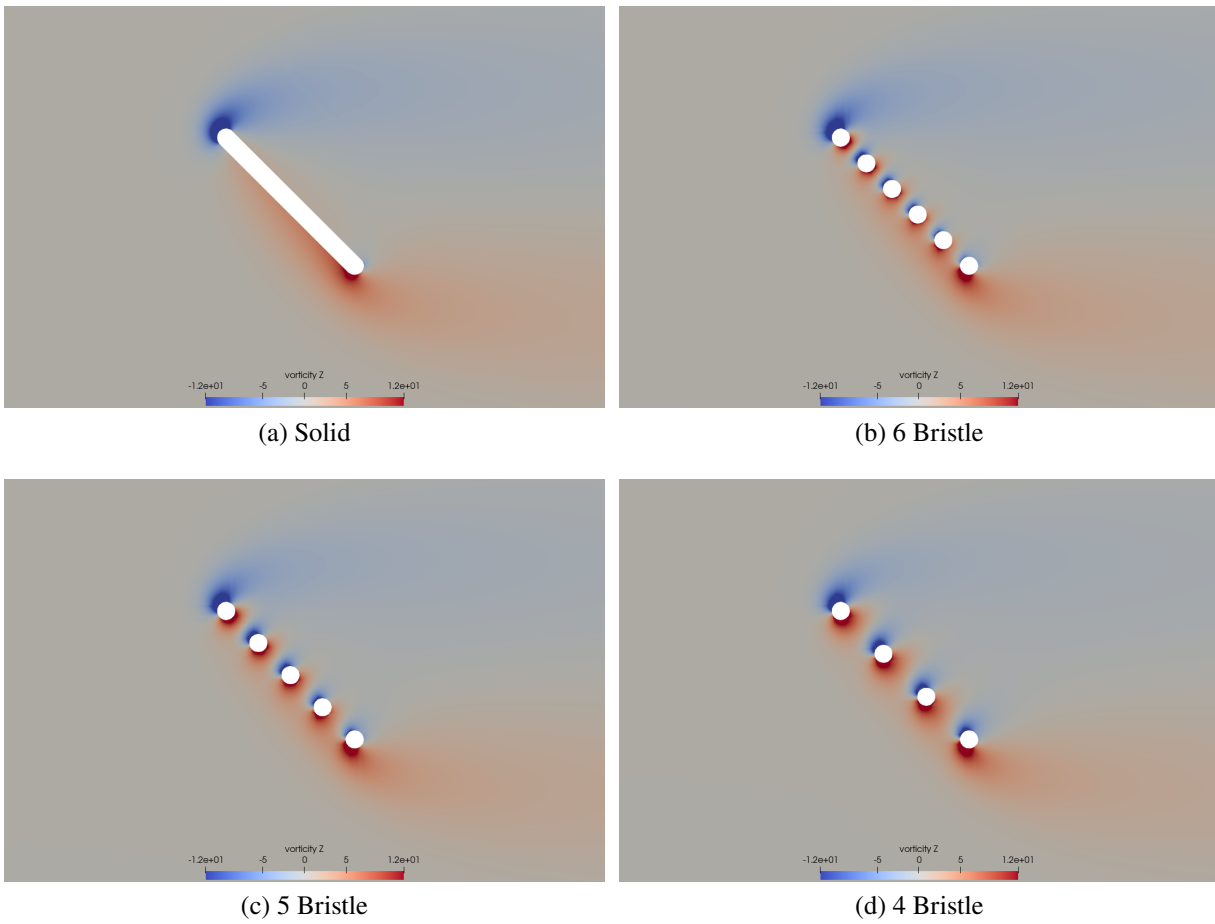


Figure 18: Vorticity Contour

Table 16: Computed values of C_d and C_l

| | Coefficient of drag (C_d) | Coefficient of lift (C_l) | C_l/C_d |
|------------|-------------------------------|-------------------------------|-----------|
| Solid Wing | 1.74205 | 1.15609 | 0.6636 |
| 6 Bristle | 1.74912 | 0.96341 | 0.5508 |
| 5 Bristle | 1.72497 | 0.76392 | 0.4429 |
| 4 Bristle | 1.65446 | 0.43698 | 0.2641 |

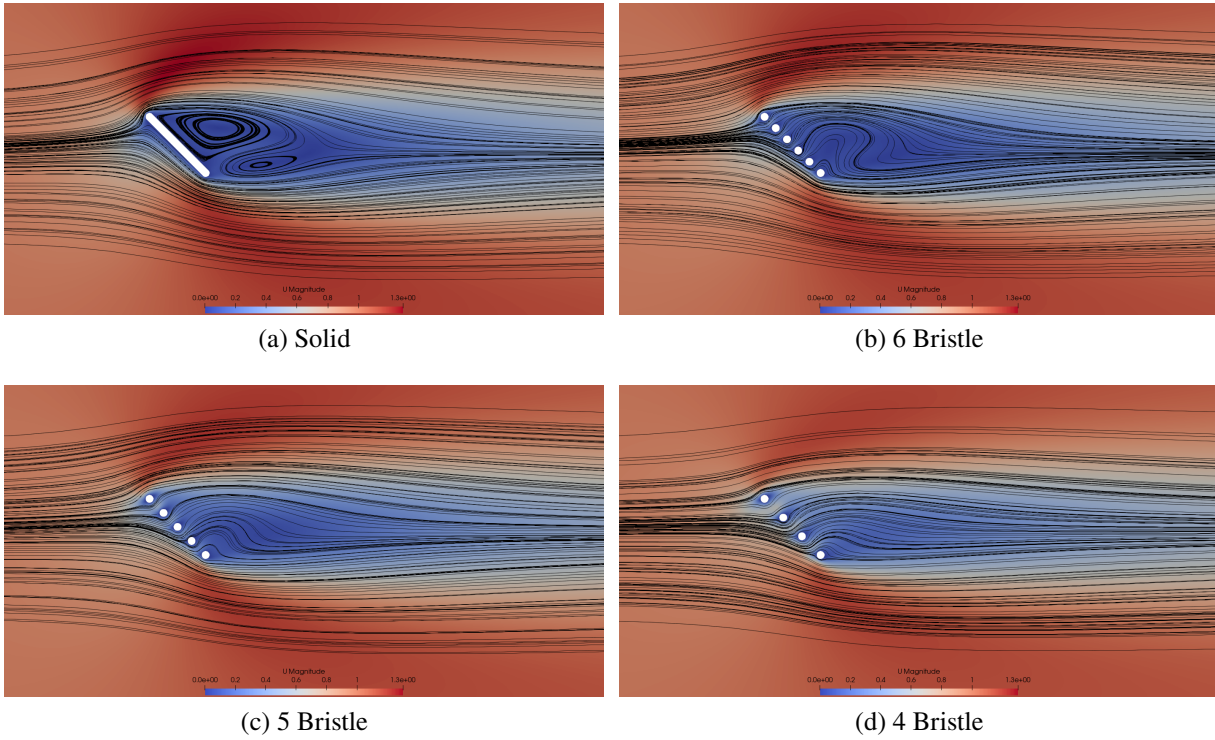


Figure 19: Velocity Contour with streamlines at 45° AOA

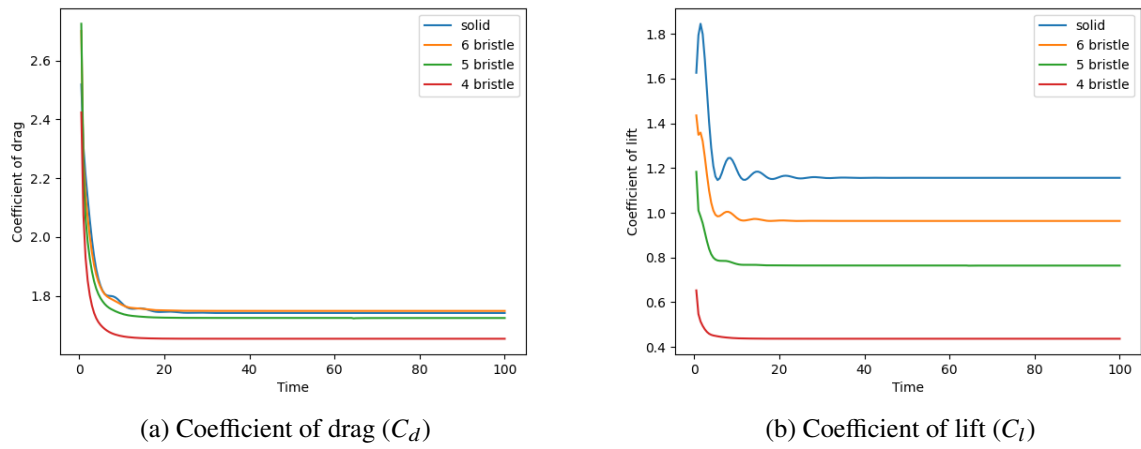


Figure 20: Comparison of force coefficients

4 Conclusions

In conclusion, the aerodynamic analysis at 90° angle of attack (AOA) demonstrates that the drag coefficient (C_d) decreases with the reduction in the number of bristles in the wing model, with the solid wing exhibiting the highest drag coefficient of 2.44599 and the four-bristle wing, the lowest at 2.16304. The streamlines and vorticity contours reveal that the solid wing generates larger counter-rotating vortices due to flow separation at the leading and trailing edges, resulting in significant drag. In contrast, bristle wings, particularly the four-bristled wing model, experience less flow separation and interference effects, allowing more fluid to pass through the gaps and reducing drag. At 45° AOA, although all models show a reduction in C_d compared to 90° AOA, the lift-to-drag ratio (C_l/C_d) varies, with the solid wing having a ratio of 0.6636, while the four-bristle wing has the lowest ratio of 0.2641. These results suggest that bristle wings are more aerodynamically efficient at high AOAs, particularly in terms of reducing drag. The 2D transient laminar simulations for both solid and bristled wing models at a low Reynolds number of 30 were completed using OpenFOAM v2112. However, the validation of the simulation setup and results has not yet been completed.

5 Acknowledgement

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References

- [1] A. Santhanakrishnan, S. K. Jones, W. B. Dickson, M. Peek, V. T. Kasoju, M. H. Dickinson, and L. A. Miller, "Flow structure and force generation on flapping wings at low reynolds numbers relevant to the flight of tiny insects," *Fluids*, vol. 3, no. 3, p. 45, 2018.
- [2] S. H. Lee, M. Lahooti, and D. Kim, "Aerodynamic characteristics of unsteady gap flow in a bristled wing," *Physics of Fluids*, vol. 30, no. 7, 2018.
- [3] S. H. Lee, M. Lee, and D. Kim, "Optimal configuration of a two-dimensional bristled wing," *Journal of Fluid Mechanics*, vol. 888, p. A23, 2020.
- [4] S. H. Lee and D. Kim, "Aerodynamic response of a bristled wing in gusty flow," *Journal of Fluid Mechanics*, vol. 913, p. A4, 2021.
- [5] Y. K. Wu, Y. P. Liu, and M. Sun, "Aerodynamics of two-dimensional bristled wings in low-reynolds-number flow," *AIP Advances*, vol. 11, no. 4, 2021.

- [6] J. Huber and J. Noyes, “A new genus and species of fairyfly, *tinkerbella nana* (hymenoptera, mymaridae), with comments on its sister genus *kikiki*, and discussion on small size limits in arthropods,” *Journal of Hymenoptera Research*, vol. 32, pp. 17–44, 2013.
- [7] S. Sunada, H. Takashima, T. Hattori, K. Yasuda, and K. Kawachi, “Fluid-dynamic characteristics of a bristled wing,” *Journal of experimental biology*, vol. 205, no. 17, pp. 2737–2744, 2002.
- [8] S. H. Lee and D. Kim, “Aerodynamics of a translating comb-like plate inspired by a fairyfly wing,” *Physics of fluids*, vol. 29, no. 8, 2017.
- [9] P. J. Roache, “Quantification of uncertainty in computational fluid dynamics,” *Annual review of fluid Mechanics*, vol. 29, no. 1, pp. 123–160, 1997.
- [10] B. Rajani, A. Kandasamy, and S. Majumdar, “Numerical simulation of laminar flow past a circular cylinder,” *Applied Mathematical Modelling*, vol. 33, no. 3, pp. 1228–1247, 2009.
- [11] A. Cheer, S. Cheung, T.-C. Hung, R. H. Piedrahita, and S. L. Sanderson, “Computational fluid dynamics of fish gill rakers during crossflow filtration,” *Bulletin of mathematical biology*, vol. 74, pp. 981–1000, 2012.
- [12] S. K. Jones, Y. J. Yun, T. L. Hedrick, B. E. Griffith, and L. A. Miller, “Bristles reduce the force required to ‘fling’ wings apart in the smallest insects,” *Journal of Experimental Biology*, vol. 219, no. 23, pp. 3759–3772, 2016.